## Preliminary Stormwater Management Study

for

# 2934-2950 Atlanta Rd Mixed-Use

LOCATED IN Land Lot No. 559, 17<sup>th</sup> District, 2<sup>nd</sup> Section City of Smyrna Cobb County, Georgia

Developer: **Tanalta Real Estate** 1425 Ellsworth Industrial Blvd, Suite 30 Atlanta, GA 30318

Engineer: **DOULGERAKIS CONSULTING ENGINEERS, INC.** 400 Abbey Ct. Alpharetta, GA 30004 (770) 753-9800

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### **REVISION SUMMARY**

Revision	Date	Description

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## **Letter to Reviewers**

Ladies and Gentlemen:

The following is the Preliminary Stormwater Management Study for Tanalta Real Estate's Mixed-Use Development located in Land Lot 559 of the 17<sup>th</sup> District, 2<sup>nd</sup> Section of the City of Smyrna, Cobb County, Georgia. The site address is 2934-2950 Atlanta Rd and it is located at the northwest corner of the intersection of Atlanta Rd and Church St. This project will combine three lots totaling 1.05 acres and redevelop the property with a four-story mixed-use building and associated parking deck. The building will be composed of office and commercial on the ground level and multifamily residential above.

The purpose of this report is to demonstrate that mitigating measures will be designed to meet the City of Smyrna requirements for Stormwater Management for the proposed development. The analysis herein is performed using the SCS method to generate hydrographs based on a 24 hour, type II distribution storm event. The study is based on the methodology outlined in the Georgia Stormwater Management Manual.

Please let us know if you should have any questions regarding this study.

Sincerely,

Emmanuel Doulgerakis, MSCE, P.E.

## **Project Narrative**

The purpose of this report is to show that mitigating measures for the proposed development will be designed to meet the City of Smyrna Requirements for the detention and water quality/runoff reduction. The project site is 1.05 acres and is located in Land Lot 559 of the 17th District, 2<sup>nd</sup> Section of the City of Smyrna, Cobb County, Georgia.

The existing conditions are three lots, one of which is vacant. The other two lots have two commercial buildings and associated parking lots. The property does not appear to contain any existing trees. Runoff generally flows from west to east towards Atlanta Rd. Runoff flows overland across the site where it is collected in drop inlets at two location (Study Points A and B) near the right of way. It then continues in the existing storm sewer system under Atlanta Rd. There are no existing detention facilities on site.

Study Point A is located in the existing 24" storm sewer located in the Atlanta Rd ROW along the northeastern half of the property. Study Point B is located in the existing 24" storm sewer located in the Atlanta Rd ROW along the southeastern half of the property. The flows from the two study points are then piped under Atlanta Rd where they combine before continuing east under the Publix shopping center. The combination point is also the 10% Study Point.

A small amount of off site area drains into the site from the neighboring church to the west.

Stormwater management for the site will be provided by constructing two underground detention/infiltration ponds, one for each study point. Water quality requirements for the site are intended to be met by providing runoff reduction in the form of infiltration for the first 1 inch of rainfall draining to the underground detention pond. The Georgia Stormwater Management Manual Stormwater Quality Site Development Review Tool is used for calculating the required water quality/runoff reduction volumes (reference Appendix D). The Tool is also used for calculating the Adjusted Curve Number for the drainage area resulting from implementing runoff reduction practices.

Field testing will need to be performed during final design to assess the suitability of the subsurface conditions for infiltration. If the infiltration test results are not suitable then an alternative BMP will be proposed for the site to satisfy the City's requirement for Runoff Reduction/Water Quality.

According to FIRM Panels 13067C0119H dated March 4, 2013 this site is not located within the 100 year flood plain.

## **Pre Development Conditions**

The existing conditions are developed land with two commercial buildings, driveways and parking lots. Per the NRCS soil maps the soil types located in this area are Urban Land – Madison, UhC. The hydrological soil type for this classification is technically unrated, however in their natural state Madison soils are of hydrological Type B, therefore Type B will be used for this analysis (Reference Appendix B). For curve number determination based on land cover reference Table 3.1.5-1 of the GSWMM. Time of concentration is calculated using the TR-55 method and calculations can be found in the Hydraflow Hydrographs Report Appendix E. Small, developed areas that are very steep and/or mostly impervious surfaces are assigned the smallest time of concentration of 6 minutes. Reference Appendix H for Pre and Post Development Maps and Appendix I for the 10% Basin Map.

Area #	Total Area (AC)	Weighted Curve Number	Time of Conc. Tc (min)	Impervious Area (AC)	Pervious Area (AC)
Curve Number		-		98	61
Area A1 On Site	0.31	94	6	0.28	0.03
Area A2 On Site	0.45	68	13.5	0.09	0.36
Area A3 <u>Off Site</u>	0.12	73	6	0.04	0.08
Area B1 On Site	0.29	97	6	0.28	0.01
Area B2 <u>Off Site</u>	0.05	76	6	0.02	0.03
Total Study Area	1.22				

## **Post Development Conditions**

The project site will be developed with a new mixed-use building, parking lots and landscaped areas. Time of concentration is calculated using the TR-55 method and calculations can be found in the Hydraflow Hydrographs Report Appendix E. Small, developed areas that are very steep and/or mostly impervious surfaces are assigned the smallest time of concentration of 6 minutes.

Area #	Total Area (AC)	Weighted Curve Number	Time of Conc. Tc (min)	Impervious Area (AC)	Pervious Area (AC)	Adjusted CN
Curve Number		-		98	61	-
Area A1 On Site	0.52	90	6	0.41	0.11	84*
Area A3 <u>Off Site</u>	0.12	73	6	0.04	0.08	-
Area B1 On Site	0.53	90	6	0.41	0.12	83*
Area B2 Off Site	0.05	76	6	0.02	0.03	-

Total Study Area 1.22

\*see curve number adjustment for runoff reduction section of this report.

## **Curve Number Adjustment for Runoff Reduction**

In accordance with the GSWMM credit can be taken in the form of a Curve Number adjustment for runoff reduction created by green infrastructure BMPs such as underground detention ponds with infiltration.

Using the SCS method, the runoff volume of the storm event (Q) may be subtracted by the runoff reduction volume (R). Using this new storm volume, an adjusted Curve Number (CNadj) can be back-calculated.

- RRv adjusted CN (assume P is equal for both adjusted and unadjusted Q)
- SCS method (unadjusted),  $Q=(P-0.2 \times S0)^2/(P+0.8 \times S0)$ ; S0 = 1000/CN -10
- SCS method (adjusted),  $Q-R=(P-0.2 \times S1)^2/(P+0.8 \times S1)$ ; S1 = 1000/CNadj 10
- R = sum of runoff reduction from all systems within the drainage area *(see pond design section)*
- P = rainfall (in)
- CN = curve number
- CNadj = adjusted curve number
- S0 = potential maximum soil moisture retention (in) based on original CN
- S1 = potential maximum soil moisture retention (in) based on CNadj

			Area	<b>SO</b>				<b>S1</b>		CN
Area	Year	CN	(sf)	(in)	P (in)	Q (cf)	R (cf)	(in)	Q-R	adj
A1	100	90.17	22651	1.09	7.54	12031	1434	1.95	10597	84
B1	100	89.62	23087	1.16	7.54	12138	1436	2.02	10702	83

For simplicity of calculations, the 100 year storm Adjusted CN was used in the hydrograph model for <u>all</u> storm events. This is a conservative approach because the 100 year adjusted CN is larger than the 2 thru 50 year adjusted CN values.

## **Sizing Criteria for Detention Ponds**

Water Quality/Runoff Reduction utilizes the equations 3.1.19 and 3.1.20 of Volume 2, Section 3.1.7.1 of the GSWMM. Runoff reduction is to be provided for the 1" storm to the maximum extent practicable. Any remaining volume is to addressed using traditional Water Quality methods for the 1.2" storm.

Stream Channel Protection utilizes the equations and methodology from GSWMM section 3.3.5 to provide extended detention for the 1-year, 24-hour storm event. Per the GSWMM Section 2.2.4.2 Stream Channel Protection is not required if the 1-year, 24-hour pond outflow to less than 2 cfs. Per section 2.2.2.2 Stream Channel Protection may be exempted if the site discharges directly into a piped stormwater drainage system and a reduction of the smaller flows will not have an impact on the stream channel integrity.

Over-bank Flood Protection was provided for by ensuring that the post development peak rate is reduced by 10% from the pre development peak rate for the 2, 10, and 25 year frequency storm events.

Extreme Flood Protection is provided for by ensuring that the post development peak rate is reduced by 10% from the pre development peak rate for the 50 and 100 year frequency storm events.

## **Design of Pond A**

Pond A is a proposed underground detention pond which receives runoff from onsite drainage area A1 and offsite area A3. The pond will be composed of three 110 LF barrels of 30" CMP with stone backfill. Two of the barrels will be perforated pipe to allow for infiltration, while the third barrel will be solid wall with an internal baffle wall serving as a pretreatment mechanism to trap sediment and debris from influent prior to entering the perforated section of the pipe. The lower portion of the pond will drain via infiltration to meet the water quality requirements for the project. The upper portion of the pond will drain via the outlet works described below to satisfy the detention requirements. Reference Appendix J for Pond Details.

Stage	Elevation	Pond Volume					
(ft)	(ft)	(cuft)					
0.00	1053.30	0					
0.51	1053.81	45					
1.02	1054.32	255					
1.53	1054.83	543					
2.04	1055.34	940					
2.55	1055.85	1,424					
2.70	1056.00*	1,577*					
3.06	1056.36	1,935					
3.57	1056.87	2,417					
4.08	1057.38	2,812					
4.59	1057.89	3,106					
5.10	1058.40	3,375					

Pond	Stage	/Storage	Table	:

Pond Elevation/Storage/Discharge Table							
Storm	Elevation	Volume	Discharge				
Event	(ft)	(cf)	(cfs)				
2 YR	1056.69	2,235	1.85				
10 YR	1056.99	2,499	2.86				
25 YR	1057.26	2,709	3.41				
50 YR	1057.45	2,822	4.24				
100 YR	1057.60	2,921	5.12				

\*Storage below this point is drained via infiltration (see Runoff Reduction/Water Quality Design below). Bottom of stone elevation at Pond low point = 1053.30 Top of Stone elevation at Pond low point = 1057.30

Downstream Invert of 30" CMP = 1054.30

Slope of detention pipe = 1.0%

#### The outlet works consists of:

15" outlet pipe at invert elevation 1056.00 and 1.0% slope (n=0.013)

<u>The 100-year ponding elevation is 1057.60.</u> The lowest point of overflow in parking lot is +/- 1058.0.

#### **Runoff Reduction/Water Quality Design:**

The pond has been sized to capture the first 1" of rainfall on Area A1 below the outlet and infiltrate it into the ground in 48 hours or less. This Runoff Reduction Volume, RRv = 1.0" x (0.05+0.009\*I%) x A / 12 x 43560.

Area Description	AREA (acres)	IMPERVIOUS (acres)	۱%	Required RRv (CF)
A1	0.52	0.41	78.85	1434

Infiltration Practices:

Description	Surface Area (SF)	i_soil (ft/day)	RRv Provided (cf)	Time To Infiltrate (hrs)	Req'd Forebay Volume (cf)	Provided Forebay Volume (cf)
Detention Pond	1165	1.00**	1577	32.49	149	270

i\_soil is from Geotech Report Appendix F

RRv is from pond stage/storage data Appendix E

Time to Drain = Volume/(i\_soil x bottom surface area)

Time to Drain must be less than 48 hours.

Forebay Volume Required (cf) = 0.1" x Imp Area x 43560 / 12

\*\*Infiltration testing is required to confirm that a minimum i = 1.0ft/day = 0.5 in/hr can be achieved at the site.

#### **Channel Protection Design Pond:**

Per the GSWMM Section 2.2.4.2 Stream Channel Protection is not required if the 1-year, 24-hour pond outflow to less than 2 cfs. Per section 2.2.2.2 Stream Channel Protection may be exempted if the site discharges directly into a piped stormwater drainage system and a reduction of the smaller flows will not have an impact on the stream channel integrity.

## **Design of Pond B**

Pond B is a proposed underground detention pond which receives runoff from onsite drainage area B1 and offsite area B2. The pond will be composed of seven 70 LF barrels of 30" CMP with stone backfill. Six of the barrels will be perforated pipe to allow for infiltration, while the seventh barrel will be solid wall with an internal baffle wall serving as a pretreatment mechanism to trap sediment and debris from infiltration to entering the perforated section of the pipe. The lower portion of the pond will drain via infiltration to meet the water quality requirements for the project. The upper portion of the pond will drain via the outlet works described below to satisfy the detention requirements. Reference Appendix J for Pond Details.

Stage	Elevation	Pond Volume				
(ft)	(ft)	(cuft)				
0.00	1051.60	0				
0.47	1052.07	124				
0.94	1052.54	463				
1.41	1053.01	831				
1.88	1053.48	1,225				
2.35	1053.95	1,783				
2.50	1054.10*	1,986*				
2.82	1054.42	2,457				
3.29	1054.89	3,165				
3.76	1055.36	3,850				
4.23	1055.83	4,438				
4.70	1056.30	4,855				

Pond Elevation/Storage/Discharge Table							
Storm Event	Elevation (ft)	Volume (cf)	Discharge (cfs)				
2 YR	1054.85	3,089	1.16				
10 YR	1055.20	3,597	1.82				
25 YR	1055.47	3,970	2.20				
50 YR	1055.72	4,285	2.45				
100 YR	1056.04	4,591	2.94				

#### Pond Stage/Storage Table:

\*Storage below this point is drained via infiltration (see Runoff Reduction/Water Quality Design below). Bottom of stone elevation at Pond low point = 1051.60 Top of Stone elevation at Pond low point = 1055.60 Downstream Invert of 30" CMP = 1053.10

Slope of detention pipe = 1.0%

#### The outlet works consists of:

15" outlet pipe at invert elevation 1054.10 and 1.0% slope (n=0.013) 12" orifice at invert elevation 1054.1 (drains to 15" outlet pipe)

<u>The 100-year ponding elevation is 1056.04.</u> <u>The lowest point of overflow in parking lot is +/- 1056.49.</u>

#### **Runoff Reduction/Water Quality Design:**

The pond has been sized to capture the first 1" of rainfall on Area A1 below the outlet and infiltrate it into the ground in 48 hours or less. This Runoff Reduction Volume, RRv = 1.0" x (0.05+0.009\*I%) x A / 12 x 43560.

Area Description	AREA (acres)	IMPERVIOUS (acres)	۱%	Required RRv (CF)
B1	0.53	0.41	77.36	1436

Infiltration Practices:

Description	Surface Area (SF)	i_soil (ft/day)	RRv Provided (cf)	Time To Infiltrate (hrs)	Req'd Forebay Volume (cf)	Provided Forebay Volume (cf)
Detention Pond	1739	1.0	1986	27.41	149	172

i\_soil is from Geotech Report <del>Appendix F</del>

*RRv is from pond stage/storage data Appendix E* 

Time to Drain = Volume/(i\_soil x bottom surface area)

Time to Drain must be less than 48 hours.

Forebay Volume Required (cf) = 0.1" x Imp Area x 43560 / 12

\*\*Infiltration testing is required to confirm that a minimum i = 1.0ft/day = 0.5 in/hr can be achieved at the site.

#### **Channel Protection Design Pond:**

Per the GSWMM Section 2.2.4.2 Stream Channel Protection is not required if the 1-year, 24-hour pond outflow to less than 2 cfs. Per section 2.2.2.2 Stream Channel Protection may be exempted if the site discharges directly into a piped stormwater drainage system and a reduction of the smaller flows will not have an impact on the stream channel integrity.

Summary of Peak Flows Per the City of Smyrna Stormwater Ordinance post development flows must be reduced by 10% from the pre-development flows leaving the development site. This analysis must be performed for the 2, 10, 25, 50, and 100-year storm events. Reference Appendix E for the complete hydrograph report.

_	Storm Frequency						
Study Point	2	10.000		EQ year	100		
A	z year	10 year	25 year	50 year	100 year		
$\mathbf{Q}_{pre}$	2.15	3.38	4.25	4.96	5.71		
Q Reqd	1.93	3.05	3.83	4.46	5.14		
Q post	2.56	3.79	4.61	5.27	5.96		
Q post adj	2.17	3.39	4.23	4.90	5.59		
<b>Q</b> Post Routed	1.85	2.86	3.41	4.24	5.12		
% Reduction	14%	15%	20%	14%	10%		

	Storm Frequency						
Study Point							
В	2 year	10 year	25 year	50 year	100 year		
Q <sub>pre</sub>	1.60	2.24	2.67	3.01	3.37		
Q Reqd	1.44	2.01	2.40	2.71	3.03		
Qpost	2.46	3.59	4.34	4.94	5.57		
Q post adj	2.00	3.12	3.88	4.49	5.12		
QPost Routed	1.16	1.82	2.20	2.45	2.94		
% Reduction	28%	18%	17%	19%	13%		

## **Downstream Analysis**

TBD. This section will be completed during final design.

	Storm Frequency					
10% Study Point	1 year	2 year	5 year	10 year	25 year	100 year
Qpre						
Qpost						
% Reduction						

## Appendix A: Location Map





Conservation Service

Web Soil Survey National Cooperative Soil Survey



## Hydrologic Soil Group

	1	1		
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
MsD3	Madison and Pacolet soils, 10 to 15 percent slopes, severely eroded	В	6.0	7.8%
MsE2	Madison and Pacolet soils, 15 to 25 percent slopes, eroded	В	0.4	0.5%
UfC	Urban land-Cecil complex, 2 to 10 percent slopes		8.8	11.4%
UhC	Urban land-Madison complex, 2 to 10 percent slopes		61.8	80.2%
Totals for Area of Intere	est		77.0	100.0%

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## **Rating Options**

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



NOAA Atlas 14, Volume 9, Version 2 Location name: Smyrna, Georgia, USA\* Latitude: 33.8823°, Longitude: -84.5137° Elevation: 1056.66 ft\*\* \* source: ESRI Maps \*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF\_tabular | PF\_graphical | Maps\_&\_aerials

#### **PF** tabular

PDS-I	S-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup>									
Duration		Average recurrence interval (years)								
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	<b>0.405</b>	<b>0.465</b>	<b>0.567</b>	<b>0.656</b>	<b>0.785</b>	<b>0.889</b>	<b>0.997</b>	<b>1.11</b>	<b>1.27</b>	<b>1.39</b>
	(0.322-0.505)	(0.370-0.580)	(0.450-0.709)	(0.518-0.823)	(0.602-1.01)	(0.665-1.16)	(0.722-1.32)	(0.773-1.50)	(0.849-1.74)	(0.907-1.93)
10-min	<b>0.593</b>	<b>0.681</b>	<b>0.831</b>	<b>0.961</b>	<b>1.15</b>	<b>1.30</b>	<b>1.46</b>	<b>1.63</b>	<b>1.86</b>	<b>2.04</b>
	(0.472-0.739)	(0.541-0.849)	(0.659-1.04)	(0.758-1.21)	(0.881-1.48)	(0.974-1.69)	(1.06-1.93)	(1.13-2.19)	(1.24-2.55)	(1.33-2.82)
15-min	<b>0.723</b>	<b>0.830</b>	<b>1.01</b>	<b>1.17</b>	<b>1.40</b>	<b>1.59</b>	<b>1.78</b>	<b>1.98</b>	<b>2.27</b>	<b>2.49</b>
	(0.576-0.901)	(0.660-1.04)	(0.803-1.27)	(0.924-1.47)	(1.07-1.81)	(1.19-2.06)	(1.29-2.35)	(1.38-2.67)	(1.52-3.11)	(1.62-3.44)
30-min	<b>1.03</b>	<b>1.18</b>	<b>1.44</b>	<b>1.67</b>	<b>1.99</b>	<b>2.26</b>	<b>2.53</b>	<b>2.82</b>	<b>3.22</b>	<b>3.54</b>
	(0.820-1.28)	(0.940-1.47)	(1.14-1.80)	(1.31-2.09)	(1.53-2.57)	(1.69-2.93)	(1.83-3.35)	(1.96-3.80)	(2.16-4.43)	(2.31-4.90)
60-min	<b>1.33</b>	<b>1.52</b>	<b>1.85</b>	<b>2.14</b>	<b>2.57</b>	<b>2.91</b>	<b>3.28</b>	<b>3.66</b>	<b>4.20</b>	<b>4.63</b>
	(1.06-1.66)	(1.21-1.90)	(1.47-2.31)	(1.69-2.68)	(1.97-3.31)	(2.18-3.79)	(2.37-4.34)	(2.55-4.94)	(2.81-5.77)	(3.02-6.40)
2-hr	<b>1.63</b>	<b>1.86</b>	<b>2.26</b>	<b>2.62</b>	<b>3.14</b>	<b>3.57</b>	<b>4.02</b>	<b>4.50</b>	<b>5.18</b>	<b>5.72</b>
	(1.31-2.01)	(1.50-2.29)	(1.81-2.79)	(2.09-3.24)	(2.44-4.01)	(2.71-4.59)	(2.95-5.27)	(3.18-6.01)	(3.52-7.04)	(3.78-7.82)
3-hr	<b>1.83</b>	<b>2.07</b>	<b>2.51</b>	<b>2.90</b>	<b>3.48</b>	<b>3.96</b>	<b>4.47</b>	<b>5.01</b>	<b>5.78</b>	<b>6.39</b>
	(1.48-2.23)	(1.68-2.54)	(2.03-3.08)	(2.33-3.57)	(2.73-4.43)	(3.03-5.07)	(3.31-5.82)	(3.57-6.65)	(3.96-7.81)	(4.26-8.69)
6-hr	<b>2.25</b>	<b>2.53</b>	<b>3.02</b>	<b>3.47</b>	<b>4.14</b>	<b>4.70</b>	<b>5.29</b>	<b>5.93</b>	<b>6.83</b>	<b>7.56</b>
	(1.84-2.72)	(2.07-3.06)	(2.47-3.67)	(2.82-4.22)	(3.29-5.21)	(3.65-5.95)	(3.98-6.82)	(4.29-7.78)	(4.76-9.14)	(5.12-10.2)
12-hr	<b>2.79</b>	<b>3.11</b>	<b>3.68</b>	<b>4.19</b>	<b>4.95</b>	<b>5.58</b>	<b>6.25</b>	<b>6.97</b>	<b>7.98</b>	<b>8.79</b>
	(2.32-3.33)	(2.58-3.72)	(3.05-4.42)	(3.45-5.04)	(3.98-6.15)	(4.39-6.98)	(4.76-7.95)	(5.11-9.03)	(5.64-10.5)	(6.05-11.7)
24-hr	<b>3.35</b>	<b>3.78</b>	<b>4.51</b>	<b>5.14</b>	<b>6.05</b>	<b>6.78</b>	<b>7.54</b>	<b>8.34</b>	<b>9.43</b>	<b>10.3</b>
	(2.81-3.96)	(3.17-4.47)	(3.77-5.34)	(4.28-6.11)	(4.91-7.38)	(5.39-8.35)	(5.81-9.45)	(6.19-10.6)	(6.76-12.3)	(7.19-13.5)
2-day	<b>3.86</b> (3.29-4.51)	<b>4.44</b> (3.77-5.19)	<b>5.40</b> (4.57-6.32)	<b>6.20</b> (5.23-7.28)	<b>7.33</b> (6.01-8.81)	<b>8.21</b> (6.59-9.96)	<b>9.10</b> (7.10-11.2)	<b>10.0</b> (7.54-12.6)	<b>11.3</b> (8.18-14.5)	<b>12.2</b> (8.66-15.9)
3-day	<b>4.24</b>	<b>4.81</b>	<b>5.80</b>	<b>6.64</b>	<b>7.86</b>	<b>8.83</b>	<b>9.84</b>	<b>10.9</b>	<b>12.3</b>	<b>13.5</b>
	(3.63-4.91)	(4.12-5.59)	(4.95-6.74)	(5.64-7.75)	(6.51-9.41)	(7.16-10.7)	(7.75-12.1)	(8.28-13.7)	(9.06-15.8)	(9.66-17.4)
4-day	<b>4.56</b> (3.93-5.27)	<b>5.13</b> (4.42-5.93)	<b>6.12</b> (5.26-7.08)	<b>7.00</b> (5.98-8.12)	<b>8.28</b> (6.92-9.90)	<b>9.33</b> (7.63-11.3)	<b>10.4</b> (8.29-12.8)	<b>11.6</b> (8.90-14.5)	<b>13.3</b> (9.82-16.9)	<b>14.6</b> (10.5-18.7)
7-day	<b>5.40</b> (4.70-6.17)	<b>6.02</b> (5.24-6.89)	<b>7.13</b> (6.19-8.17)	<b>8.14</b> (7.02-9.35)	<b>9.65</b> (8.17-11.5)	<b>10.9</b> (9.03-13.0)	<b>12.3</b> (9.86-14.9)	<b>13.7</b> (10.6-17.0)	<b>15.8</b> (11.8-19.9)	<b>17.4</b> (12.7-22.2)
10-day	<b>6.12</b> (5.36-6.95)	<b>6.81</b> (5.97-7.74)	<b>8.04</b> (7.02-9.15)	<b>9.16</b> (7.96-10.5)	<b>10.8</b> (9.24-12.8)	<b>12.2</b> (10.2-14.5)	<b>13.7</b> (11.1-16.6)	<b>15.3</b> (12.0-18.9)	<b>17.6</b> (13.3-22.2)	<b>19.5</b> (14.4-24.6)
20-day	<b>8.18</b> (7.26-9.17)	<b>9.05</b> (8.02-10.1)	<b>10.6</b> (9.34-11.9)	<b>11.9</b> (10.5-13.4)	<b>13.9</b> (12.0-16.1)	<b>15.5</b> (13.1-18.1)	<b>17.2</b> (14.1-20.5)	<b>19.0</b> (15.1-23.1)	<b>21.5</b> (16.5-26.6)	<b>23.5</b> (17.6-29.4)
30-day	<b>10.0</b> (8.96-11.1)	<b>11.1</b> (9.88-12.3)	<b>12.8</b> (11.4-14.3)	<b>14.3</b> (12.7-16.0)	<b>16.5</b> (14.3-18.9)	<b>18.2</b> (15.4-21.0)	<b>19.9</b> (16.5-23.5)	<b>21.8</b> (17.4-26.2)	<b>24.3</b> (18.8-29.8)	<b>26.2</b> (19.9-32.5)
45-day	<b>12.5</b> (11.3-13.8)	<b>13.8</b> (12.4-15.3)	<b>15.9</b> (14.3-17.6)	<b>17.6</b> (15.8-19.6)	<b>20.0</b> (17.4-22.6)	<b>21.8</b> (18.6-24.9)	<b>23.5</b> (19.6-27.4)	<b>25.3</b> (20.4-30.1)	<b>27.6</b> (21.6-33.5)	<b>29.4</b> (22.5-36.2)
60-day	<b>14.8</b> (13.4-16.2)	<b>16.3</b> (14.8-17.9)	<b>18.7</b> (16.9-20.6)	<b>20.7</b> (18.6-22.8)	<b>23.2</b> (20.2-26.0)	<b>25.0</b> (21.5-28.4)	<b>26.8</b> (22.4-30.9)	<b>28.5</b> (23.0-33.6)	<b>30.6</b> (24.0-36.8)	<b>32.0</b> (24.7-39.2)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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**PF graphical** 





Duration						
5-min	2-day					
10-min	— 3-day					
15-min	— 4-day					
30-min	- 7-day					
- 60-min	— 10-day					
— 2-hr	- 20-day					
— 3-hr	— 30-day					
— 6-hr	— 45-day					
- 12-hr	- 60-day					
24-hr						

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Maps & aerials

Small scale terrain



Large scale terrain





Large scale aerial



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US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

**Disclaimer** 







### Georgia Stormwater Management Manual Stormwater Quality Site Development Review Tool, v2.2

Development Name: 2934-2950 Atlanta Rd Mixed Use

data input cells calculation cells constant values

Drainage Basin Name: Area A1 and A2

#### Channel and Flood Protection Calculations

	1-yr, 24-hr	2-yr, 24-hr	25-yr, 24-hr	100-yr, 24-hr
	storm	storm	storm	storm
Target Rainfall Event (in)	3.35	3.78	6.05	7.54

	1-yr, 24-hr	2-yr, 24-hr	25-yr, 24-hr	100-yr, 24-hr
	storm	storm	storm	storm
Pre-Development Runoff Volume (in)	1.45	1.79	3.73	5.08
Post Development Runoff Volume (in) with no BMPs	2.32	2.73	4.91	6.37
Post-Development Runoff Volume (in) with BMPs	1.56	1.97	4.15	5.61
Adjusted CN	81	81	83	84

\*See Stormwater Management Standards to Determine Detention Requirements.

Comments





### Georgia Stormwater Management Manual Stormwater Quality Site Development Review Tool, v2.2

Development Name: 2934-2950 Atlanta Rd Mixed Use

data input cells calculation cells constant values

Drainage Basin Name: Area B1

#### Channel and Flood Protection Calculations

	1-yr, 24-hr	2-yr, 24-hr	25-yr, 24-hr	100-yr, 24-hr
	storm	storm	storm	storm
Target Rainfall Event (in)	3.35	3.78	6.05	7.54

	1-yr, 24-hr	2-yr, 24-hr	25-yr, 24-hr	100-yr, 24-hr
	storm	storm	storm	storm
Pre-Development Runoff Volume (in)	2.98	3.40	5.66	7.15
Post Development Runoff Volume (in) with no BMPs	2.27	2.68	4.85	6.31
Post-Development Runoff Volume (in) with BMPs	1.53	1.93	4.11	5.56
Adjusted CN	80	81	83	83

\*See Stormwater Management Standards to Determine Detention Requirements.

Comments

Hyd.	Hydrograph type	Inflow				Peak Out	flow (cfs)	)			Hydrograph
NO.	(origin)	nya(s)	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr	Description
1	SCS Runoff			1.496			2.091	2.486	2.801	3.128	A1 PRE
2	SCS Runoff			0.568			1.100	1.498	1.831	2.187	A2 PRE
3	SCS Runoff			0.280			0.484	0.632	0.755	0.884	A3 PRE
4	SCS Runoff			1.469			2.014	2.378	2.669	2.972	B1 PRE
5	SCS Runoff			0.133			0.223	0.287	0.339	0.393	B2 PRE
7	SCS Runoff			2.284			3.302	3.977	4.516	5.075	A1 POST
8	SCS Runoff			1.896			2.910	3.593	4.141	4.711	A1 ADJ RR
9	SCS Runoff			2.328			3.365	4.054	4.603	5.173	B1 POST
10	SCS Runoff			1.864			2.893	3.589	4.148	4.729	B1 ADJ RR
12	Combine	1, 2, 3,		2.149			3.384	4.251	4.961	5.711	SP A PRE
13	Combine	3, 7,		2.558			3.785	4.610	5.271	5.959	SP A POST
14	Combine	3, 8,		2.170			3.393	4.226	4.896	5.594	SP A POST ADJ
15	Reservoir	14		1.852			2.863	3.411	4.242	5.119	Pond A
18	Combine	4, 5,		1.601			2.237	2.665	3.008	3.365	SP B PRE
19	Combine	5, 9,		2.460			3.588	4.341	4.942	5.566	SP B POST
20	Combine	5, 10,		1.997			3.117	3.876	4.487	5.122	SP B POST ADJ
21	Reservoir	20		1.157			1.824	2.201	2.451	2.944	POND B
<b>D</b> =1											

Proj. file: TANALTA SMYRNA.gpw

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	1.496	2	716	3,280				A1 PRE
2	SCS Runoff	0.568	2	724	1,701				A2 PRE
3	SCS Runoff	0.280	2	718	560				A3 PRE
4	SCS Runoff	1.469	2	716	3,388				B1 PRE
5	SCS Runoff	0.133	2	718	267				B2 PRE
7	SCS Runoff	2.284	2	716	4,798				A1 POST
8	SCS Runoff	1.896	2	716	3,855				A1 ADJ RR
9	SCS Runoff	2.328	2	716	4,890				B1 POST
10	SCS Runoff	1.864	2	716	3,781				B1 ADJ RR
12	Combine	2.149	2	718	5,541	1, 2, 3,			SP A PRE
13	Combine	2.558	2	716	5,358	3, 7,			SP A POST
14	Combine	2.170	2	716	4,415	3, 8,			SP A POST ADJ
15	Reservoir	1.852	2	720	4,361	14	1056.69	2,235	Pond A
18	Combine	1.601	2	716	3,655	4, 5,			SP B PRE
19	Combine	2.460	2	716	5,157	5, 9,			SP B POST
20	Combine	1.997	2	716	4,049	5, 10,			SP B POST ADJ
21	Reservoir	1.157	2	722	4,034	20	1054.85	3,089	POND B
TAI	NALTA SMYF	RNA.gpw			Return P	eriod: 2 Ye	ear	Monday, 10	) / 10 / 2022

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	2.091	2	716	4,691				A1 PRE
2	SCS Runoff	1.100	2	722	3,153				A2 PRE
3	SCS Runoff	0.484	2	718	976				A3 PRE
4	SCS Runoff	2.014	2	716	4,724				B1 PRE
5	SCS Runoff	0.223	2	716	451				B2 PRE
7	SCS Runoff	3.302	2	716	7,099				A1 POST
8	SCS Runoff	2.910	2	716	6,014				A1 ADJ RR
9	SCS Runoff	3.365	2	716	7,235				B1 POST
10	SCS Runoff	2.893	2	716	5,954				B1 ADJ RR
12	Combine	3.384	2	718	8,820	1, 2, 3,			SP A PRE
13	Combine	3.785	2	716	8,075	3, 7,			SP A POST
14	Combine	3.393	2	716	6,991	3, 8,			SP A POST ADJ
15	Reservoir	2.863	2	720	6,936	14	1056.99	2,499	Pond A
18	Combine	2.237	2	716	5,175	4, 5,			SP B PRE
19	Combine	3.588	2	716	7,686	5, 9,			SP B POST
20	Combine	3.117	2	716	6,405	5, 10,			SP B POST ADJ
21	Reservoir	1.824	2	722	6,390	20	1055.20	3,597	POND B
TAT	NALTA SMYF	RNA.gpw			Return F	eriod: 10	Year	Monday, 10	) / 10 / 2022

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	2.486	2	716	5,640				A1 PRE
2	SCS Runoff	1.498	2	722	4,235				A2 PRE
3	SCS Runoff	0.632	2	716	1,278				A3 PRE
4	SCS Runoff	2.378	2	716	5,619				B1 PRE
5	SCS Runoff	0.287	2	716	582				B2 PRE
7	SCS Runoff	3.977	2	716	8,662				A1 POST
8	SCS Runoff	3.593	2	716	7,509				A1 ADJ RR
9	SCS Runoff	4.054	2	716	8,828				B1 POST
10	SCS Runoff	3.589	2	716	7,463				B1 ADJ RR
12	Combine	4.251	2	718	11,154	1, 2, 3,			SP A PRE
13	Combine	4.610	2	716	9,940	3, 7,			SP A POST
14	Combine	4.226	2	716	8,787	3, 8,			SP A POST ADJ
15	Reservoir	3.411	2	720	8,733	14	1057.26	2,709	Pond A
18	Combine	2.665	2	716	6,202	4, 5,			SP B PRE
19	Combine	4.341	2	716	9,411	5, 9,			SP B POST
20	Combine	3.876	2	716	8,046	5, 10,			SP B POST ADJ
21	Reservoir	2.201	2	722	8,031	20	1055.47	3,970	POND B
	NALTA SMYF	RNA.gpw			Return P	eriod: 25	/ear	Monday, 10	) / 10 / 2022

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	2.801	2	716	6,404				A1 PRE
2	SCS Runoff	1.831	2	722	5,149				A2 PRE
3	SCS Runoff	0.755	2	716	1,530				A3 PRE
4	SCS Runoff	2.669	2	716	6,338				B1 PRE
5	SCS Runoff	0.339	2	716	691				B2 PRE
7	SCS Runoff	4.516	2	716	9,923				A1 POST
8	SCS Runoff	4.141	2	716	8,726				A1 ADJ RR
9	SCS Runoff	4.603	2	716	10,114				B1 POST
10	SCS Runoff	4.148	2	716	8,694				B1 ADJ RR
12	Combine	4.961	2	718	13,083	1, 2, 3,			SP A PRE
13	Combine	5.271	2	716	11,453	3, 7,			SP A POST
14	Combine	4.896	2	716	10,256	3, 8,			SP A POST ADJ
15	Reservoir	4.242	2	720	10,202	14	1057.45	2,822	Pond A
18	Combine	3.008	2	716	7,030	4, 5,			SP B PRE
19	Combine	4.942	2	716	10,805	5, 9,			SP B POST
20	Combine	4.487	2	716	9,386	5, 10,			SP B POST ADJ
21	Reservoir	2.451	2	722	9,371	20	1055.72	4,285	POND B
TAI	NALTA SMYF	RNA.gpw			Return P	eriod: 50	Year	Monday, 10	) / 10 / 2022

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	3.128	2	716	7,200				A1 PRE
2	SCS Runoff	2.187	2	722	6,135				A2 PRE
3	SCS Runoff	0.884	2	716	1,799				A3 PRE
4	SCS Runoff	2.972	2	716	7,087				B1 PRE
5	SCS Runoff	0.393	2	716	807				B2 PRE
7	SCS Runoff	5.075	2	716	11,243				A1 POST
8	SCS Runoff	4.711	2	716	10,006				A1 ADJ RR
9	SCS Runoff	5.173	2	716	11,459				B1 POST
10	SCS Runoff	4.729	2	716	9,991				B1 ADJ RR
12	Combine	5.711	2	718	15,133	1, 2, 3,			SP A PRE
13	Combine	5.959	2	716	13,041	3, 7,			SP A POST
14	Combine	5.594	2	716	11,805	3, 8,			SP A POST ADJ
15	Reservoir	5.119	2	718	11,751	14	1057.60	2,921	Pond A
18	Combine	3.365	2	716	7,894	4, 5,			SP B PRE
19	Combine	5.566	2	716	12,266	5, 9,			SP B POST
20	Combine	5.122	2	716	10,798	5, 10,			SP B POST ADJ
21	Reservoir	2.944	2	722	10,783	20	1056.04	4,591	POND B
TAT	NALTA SMYF	RNA.gpw			Return P	eriod: 100	Year	Monday, 10	) / 10 / 2022

## **Hydraflow Rainfall Report**

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Return Period	Intensity-D	Intensity-Duration-Frequency Equation Coefficients (FHA)									
(Yrs)	В	D	E	(N/A)							
1	0.0000	0.0000	0.0000								
2	29.6471	7.7000	0.6926								
3	0.0000	0.0000	0.0000								
5	29.2182	5.1000	0.6305								
10	40.3921	6.3000	0.6731								
25	49.1053	6.9000	0.6815								
50	66.1182	8.6000	0.7237								
100	62.1387	7.5000	0.6898								

File name: atlanta.IDF

#### Intensity = B / (Tc + D)^E

Return					Intens	sity Values	(in/hr)					
(Yrs)	5 min	10	15	20	25	30	35	40	45	50	55	60
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	5.10	4.05	3.41	2.97	2.65	2.40	2.20	2.04	1.90	1.79	1.69	1.60
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	6.80	5.28	4.41	3.83	3.42	3.10	2.85	2.65	2.48	2.33	2.21	2.10
10	7.90	6.17	5.15	4.47	3.98	3.60	3.30	3.06	2.85	2.68	2.53	2.40
25	9.08	7.15	5.99	5.21	4.64	4.20	3.85	3.57	3.33	3.13	2.95	2.80
50	10.00	7.97	6.71	5.84	5.20	4.70	4.30	3.98	3.71	3.47	3.27	3.10
100	10.88	8.63	7.25	6.32	5.63	5.10	4.68	4.33	4.04	3.80	3.59	3.40

Tc = time in minutes. Values may exceed 60.

		R	ainfall F	Precipita	tion Tab	ole (in)		
Storm Distribution	1-yr	2-yr	3-yr	5-yr	10-yr	25-yr	50-yr	100-yr
SCS 24-hour	3.35	3.78	0.00	4.51	5.14	6.05	6.78	7.54
SCS 6-Hr	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-1st	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-2nd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-3rd	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-4th	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Huff-Indy	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Custom	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Precip. file name: C:\2022-06 Tanalta Smyrna\stormwater management\SMYRNA.pcp

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

### Hyd. No. 1

Hydrograph type	= SCS Runoff	Peak discharge	= 3.128 cfs
Storm frequency	= 100 yrs	Time to peak	= 716 min
Time interval	= 2 min	Hyd. volume	= 7,200 cuft
Drainage area	= 0.310 ac	Curve number	= 94*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 6.00 min
Total precip.	= 7.54 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

\* Composite (Area/CN) = [(0.030 x 61) + (0.280 x 98)] / 0.310



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

### Hyd. No. 2

Hydrograph type	= SCS Runoff	Peak discharge	= 2.187 cfs
Storm frequency	= 100 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 6,135 cuft
Drainage area	= 0.450 ac	Curve number	= 68*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= TR55	Time of conc. (Tc)	= 13.50 min
Total precip.	= 7.54 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

\* Composite (Area/CN) = [(0.360 x 61) + (0.090 x 98)] / 0.450



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## Hyd. No. 2

A2 PRE

<u>Description</u>	A		<u>B</u>		<u>C</u>		<u>Totals</u>
Sheet Flow Manning's n-value Flow length (ft) Two-year 24-hr precip. (in) Land slope (%) Travel Time (min)	= 0.240 = 100.0 = 3.97 = 2.00 = <b>12.81</b>	+	0.011 0.0 0.00 0.00 <b>0.00</b>	+	0.011 0.0 0.00 0.00 <b>0.00</b>	=	12.81
Shallow Concentrated Flow Flow length (ft) Watercourse slope (%) Surface description Average velocity (ft/s)	= 95.00 = 2.00 = Unpave =2.28	ed	0.00 0.00 Paved 0.00		0.00 0.00 Paved 0.00		
Travel Time (min)	= 0.69	+	0.00	+	0.00	=	0.69
<b>Channel Flow</b> X sectional flow area (sqft) Wetted perimeter (ft) Channel slope (%) Manning's n-value Velocity (ft/s)	= 0.00 = 0.00 = 0.00 = 0.015 =0.00		0.00 0.00 0.00 0.015 0.00		0.00 0.00 0.00 0.015 0.00		
Flow length (ft)	({0})0.0		0.0		0.0		
Travel Time (min)	= 0.00	+	0.00	+	0.00	=	0.00
Total Travel Time, Tc							

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#### Hyd. No. 3

Hydrograph type	= SCS Runoff	Peak discharge	= 0.884 cfs
Storm frequency	= 100 yrs	Time to peak	= 716 min
Time interval	= 2 min	Hyd. volume	= 1,799 cuft
Drainage area	= 0.120 ac	Curve number	= 73*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 6.00 min
Total precip.	= 7.54 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

\* Composite (Area/CN) = [(0.080 x 61) + (0.040 x 98)] / 0.120



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### Hyd. No. 4

Hydrograph type	= SCS Runoff	Peak discharge	= 2.972 cfs
Storm frequency	= 100 yrs	Time to peak	= 716 min
Time interval	= 2 min	Hyd. volume	= 7,087 cuft
Drainage area	= 0.290 ac	Curve number	= 97*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 6.00 min
Total precip.	= 7.54 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

\* Composite (Area/CN) = [(0.010 x 61) + (0.280 x 98)] / 0.290



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#### Hyd. No. 5

Hydrograph type =	SCS Runoff	Peak discharge	= 0.393 cfs
Storm frequency =	= 100 yrs	Time to peak	= 716 min
Time interval =	= 2 min	Hyd. volume	= 807 cuft
Drainage area =	= 0.050 ac	Curve number	= 76*
Basin Slope =	= 0.0 %	Hydraulic length	= 0 ft
Tc method =	= User	Time of conc. (Tc)	= 6.00 min
Total precip. =	= 7.54 in	Distribution	= Type II
Storm duration =	= 24 hrs	Shape factor	= 484

\* Composite (Area/CN) = [(0.030 x 61) + (0.020 x 98)] / 0.050



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#### Hyd. No. 7

Hydrograph type	= SCS Runoff	Peak discharge	= 5.075 cfs
Storm frequency	= 100 yrs	Time to peak	= 716 min
Time interval	= 2 min	Hyd. volume	= 11,243 cuft
Drainage area	= 0.520 ac	Curve number	= 90*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 6.00 min
Total precip.	= 7.54 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

\* Composite (Area/CN) = [(0.110 x 61) + (0.410 x 98)] / 0.520



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#### Hyd. No. 8

A1 ADJ RR

Hydrograph type	= SCS Runoff	Peak discharge	= 4.711 cfs
Storm frequency	= 100 yrs	Time to peak	= 716 min
Time interval	= 2 min	Hyd. volume	= 10,006 cuft
Drainage area	= 0.520 ac	Curve number	= 84
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 6.00 min
Total precip.	= 7.54 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 9

**B1 POST** 

Hydrograph type	= SCS Runoff	Peak discharge	= 5.173 cfs
Storm frequency	= 100 yrs	Time to peak	= 716 min
Time interval	= 2 min	Hyd. volume	= 11,459 cuft
Drainage area	= 0.530 ac	Curve number	= 90*
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 6.00 min
Total precip.	= 7.54 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484

\* Composite (Area/CN) = [(0.120 x 61) + (0.410 x 98)] / 0.530



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#### Hyd. No. 10

**B1 ADJ RR** 

Hydrograph type	= SCS Runoff	Peak discharge	= 4.729 cfs
Storm frequency	= 100 yrs	Time to peak	= 716 min
Time interval	= 2 min	Hyd. volume	= 9,991 cuft
Drainage area	= 0.530 ac	Curve number	= 83
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 6.00 min
Total precip.	= 7.54 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



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#### Hyd. No. 12

SP A PRE

Combine 100 yrs 2 min 1, 2, 3	Peak discharge Time to peak Hyd. volume Contrib. drain. area	= 5.711 cfs = 718 min = 15,133 cuft = 0.880 ac
1, 2, 3	Contrib. drain. area	= 0.880 ac
	Combine 100 yrs 2 min 1, 2, 3	CombinePeak discharge100 yrsTime to peak2 minHyd. volume1, 2, 3Contrib. drain. area



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#### Hyd. No. 13

SP A POST



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Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

#### Hyd. No. 14

SP A POST ADJ

Inflow hyds. = 3, 8 Contrib. drain. area = 0.640 ac	Hydrograph type	= Combine	Peak discharge	= 5.594 cfs
	Storm frequency	= 100 yrs	Time to peak	= 716 min
	Time interval	= 2 min	Hyd. volume	= 11,805 cuft
	Inflow hyds.	= 3, 8	Contrib. drain. area	= 0.640 ac



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#### Hyd. No. 15

Pond A

Hydrograph type	= Reservoir	Peak discharge	= 5.119 cfs
Storm frequency	= 100 yrs	Time to peak	= 718 min
Time interval	= 2 min	Hyd. volume	= 11,751 cuft
Inflow hyd. No.	= 14 - SP A POST ADJ	Max. Elevation	= 1057.60 ft
Reservoir name	= Pond A	Max. Storage	= 2,921 cuft

Storage Indication method used. Wet pond routing start elevation = 1055.95 ft.



## **Pond Report**

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

#### Pond No. 1 - Pond A

#### Pond Data

**UG Chambers -**Invert elev. = 1054.30 ft, Rise x Span =  $2.50 \times 2.50$  ft, Barrel Len = 110.00 ft, No. Barrels = 3, Slope = 1.00%, Headers = No **Encasement -**Invert elev. = 1053.30 ft, Width = 4.00 ft, Height = 4.00 ft, Voids = 40.00%

#### Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	1053.30	n/a	0	0
0.51	1053.81	n/a	45	45
1.02	1054.32	n/a	211	255
1.53	1054.83	n/a	287	543
2.04	1055.34	n/a	398	940
2.55	1055.85	n/a	483	1,424
3.06	1056.36	n/a	511	1,935
3.57	1056.87	n/a	482	2,417
4.08	1057.38	n/a	395	2,812
4.59	1057.89	n/a	294	3,106
5.10	1058.40	n/a	269	3,375

#### **Culvert / Orifice Structures**

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 15.00	0.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00
Span (in)	= 15.00	0.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 1	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 1056.00	0.00	0.00	0.00	Weir Type	=			
Length (ft)	= 23.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 1.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 0.000 (b	y Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



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#### **Weir Structures**

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

#### Hyd. No. 18

SP B PRE

Hydrograph type	<ul> <li>Combine</li> <li>100 yrs</li> <li>2 min</li> <li>4, 5</li> </ul>	Peak discharge	= 3.365 cfs
Storm frequency		Time to peak	= 716 min
Time interval		Hyd. volume	= 7,894 cuft
Inflow hyds.		Contrib. drain. area	= 0.340 ac
Inflow hyds.	= 4,5	Contrib. drain. area	= 0.340 ac
Time interval	= $2 \text{ min}$	Hyd. volume	= 7,894 cuft
Inflow hyds.	= 4, 5	Contrib. drain. area	= 0.340 ac



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Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

#### Hyd. No. 19

SP B POST

Combine 100 yrs 2 min 5, 9	Peak discharge Time to peak Hyd. volume Contrib. drain. area	= 5.566 cfs = 716 min = 12,266 cuft = 0.580 ac
5, 9	Contrib. drain. area	= 0.580 ac
	Combine 100 yrs 2 min 5, 9	CombinePeak discharge100 yrsTime to peak2 minHyd. volume5, 9Contrib. drain. area



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

#### Hyd. No. 20

SP B POST ADJ

Inflow hyds. $= 5, 10$ Tryd. volume $= 10,750$ curtInflow hyds. $= 5, 10$ Contrib. drain. area $= 0.580$ ac	Hydrograph type= CStorm frequency= 1Time interval= 2Inflow hyds.= 5	Combine 100 yrs 2 min 5, 10	Peak discharge Time to peak Hyd. volume Contrib. drain. area	= 5.122 cfs = 716 min = 10,798 cuft = 0.580 ac
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Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

#### Hyd. No. 21

POND B

Hydrograph type	= Reservoir	Peak discharge	= 2.944 cfs
Storm frequency	= 100 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 10,783 cuft
Inflow hyd. No.	= 20 - SP B POST ADJ	Max. Elevation	= 1056.04 ft
Reservoir name	= Pond B	Max. Storage	= 4,591 cuft

Storage Indication method used. Wet pond routing start elevation = 1054.09 ft.



## **Pond Report**

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

#### Pond No. 2 - Pond B

#### Pond Data

**UG Chambers -**Invert elev. = 1053.10 ft, Rise x Span =  $2.50 \times 2.50$  ft, Barrel Len = 70.00 ft, No. Barrels = 7, Slope = 1.00%, Headers = No **Encasement -**Invert elev. = 1051.60 ft, Width = 4.00 ft, Height = 4.00 ft, Voids = 40.00%

Stage	/ Storage	Table
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Stage (ft) Elevation (ft)		Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)	
0.00	1051.60	n/a	0	0	
0.47	1052.07	n/a	124	124	
0.94	1052.54	n/a	338	463	
1.41	1053.01	n/a	369	831	
1.88	1053.48	n/a	394	1,225	
2.35	1053.95	n/a	559	1,783	
2.82	1054.42	n/a	674	2,457	
3.29	1054.89	n/a	707	3,165	
3.76	1055.36	n/a	685	3,850	
4.23	1055.83	n/a	588	4,438	
4.70	1056.30	n/a	417	4,855	

#### **Culvert / Orifice Structures**

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 15.00	12.00	0.00	0.00	Crest Len (ft)	= 0.00	0.00	0.00	0.00
Span (in)	= 15.00	12.00	0.00	0.00	Crest El. (ft)	= 0.00	0.00	0.00	0.00
No. Barrels	= 1	1	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 1054.10	1054.10	0.00	0.00	Weir Type	=			
Length (ft)	= 11.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 1.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 0.000 (b	y Contour)		
Multi-Stage	= n/a	Yes	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Weir Structures





NOTES: 1. THE SOIL TYPE FOR THIS AREA IS URBAN LAND - MADISON, UhC.









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